

Lecture 26

Premixed Flame Quenching, Flammability, Ignition

Flame Extinction

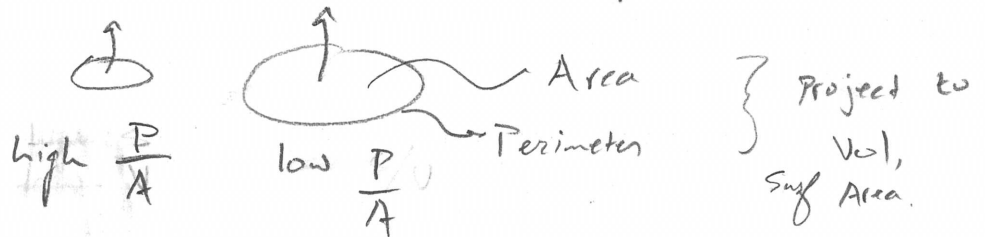
- Recall video: products/flame were cooled by Heat Transfer.
- Sprays: $\Delta H_{vap} \rightarrow$ cools by Heat Transfer.
- Chemical Suppressants: Halogens alter kinetics (Suck up radicals)
 - Use in place of Sprinklers to avoid water Damage.
 - e.g. Computer facilities.

Quenching

- Flames propagate through passages \rightarrow extinguish if passage is small

Q Main factors?

- \rightarrow Volumetric Heat release vs "Surface" Heat Transfer.
- \rightarrow Critical Diameter \rightarrow Quenching Dist.



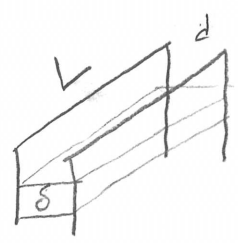
- Also Slots
- "Flame arrestors"

- $D_{Q, tube} \sim 20-50\%$ higher than $D_{Q, slit}$.

$$\left. \begin{array}{l} \infty \text{ Slits} \rightarrow \frac{P}{A} = \frac{2}{D_s} \\ \text{Circle} \rightarrow \frac{P}{A} = \frac{1}{4D_c} \end{array} \right\} \rightarrow D_c = \frac{1}{8} D_s \sim 12.5\%$$

Quenching

• Quenching Distance: Slot



• Energy Balance:

- Heat Release = Heat Transfer
- Steady State at limit just before extinction.

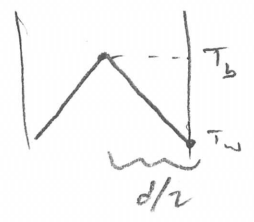
$$\dot{Q}''' \cdot V = A q''$$

$$V = L d \delta$$

$$A = 2 L \delta$$

$$\dot{Q}''' = \dot{m}_F''' \Delta h_c$$

$$q'' = \lambda \left. \frac{dT}{dx} \right|_{\text{wall}} \approx \lambda \frac{T_b - T_w}{d/2} \approx \lambda \frac{T_b - T_w}{d/b}$$



$$\dot{m}_F''' \Delta h_c \cdot \cancel{L d \delta} = \frac{2 \cancel{L} \lambda b}{d} (T_b - T_w)$$

$$* d^2 = (T_b - T_w) \cdot \frac{2 \lambda b}{\dot{m}_F''' \Delta h_c}$$

$$\Delta h_c = (1 + \nu) C_p (T_b - T_w)$$

$$F + \nu O_x \rightarrow (1 + \nu) \text{Prod}$$

$$\Delta h_c \text{ is } \frac{J}{\text{kg fuel}}$$

$$d^2 = \frac{2 \lambda b (T_b - T_w)}{\dot{m}_F''' C_p (T_b - T_w) (1 + \nu)}$$

$$d^2 = \frac{2b}{\dot{m}_F''' (1 + \nu)} \cdot \frac{\lambda \rho_u}{\rho_u C_p} = \frac{2b \alpha}{\dot{m}_F''' (1 + \nu)} = 4b \alpha^2 \cdot \frac{2 \rho_u}{2 \alpha \dot{m}_F''' (1 + \nu)} = \frac{4b \alpha^2}{S_L^2}$$

$d = \frac{2b}{S_L} \cdot \frac{2\sqrt{b}\alpha}{S_L}$

$d = \sqrt{b} \delta$

Turns' S_L

Notes: $S_L \rightarrow d = \frac{\sqrt{2b} \alpha}{S_L} = \sqrt{2b} \delta$

our in-class S_L Alternative.

- d increases with increasing α
- d decreases with increasing S_L
- $d \propto \delta$

Q Do These make Sense?

Q How Does b change w/ increasing α ?

Ex: Methane, $P=1$ atm, $\phi=1$, $T_u=300$ K.

$\rightarrow S_L = 40$ cm/s

$\rightarrow d = 2\sqrt{b} \left(2.26 \times 10^{-4} \frac{m^2}{s} \right) / 0.41 \text{ m/s} = 5.69 \times 10^{-4} \cdot 2\sqrt{b} \text{ m}$

Table 8.4 $\rightarrow d = 0.0025$ m

w/ $\alpha = 3.24 \times 10^{-4}$
 $b = 2.38$

$\rightarrow b = 4.9$

Alternate $\rightarrow b = 9.8$

Note: b is unknown! \rightarrow relations give order of magnitude of d , not functional form. $b > 2$ is true.

Ignition Energy

- Spherical Spark: Again at extinction limit.
- SS.



- Some Analysis.

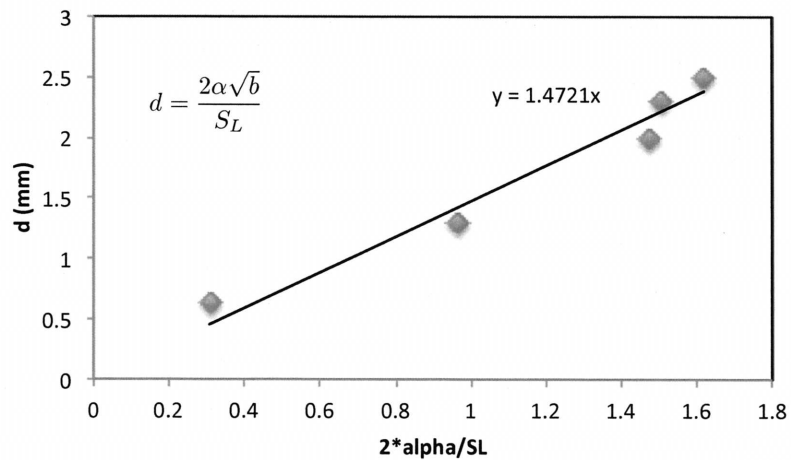
$\dot{m}_F''' \cdot \Delta h_c \cdot V = -\lambda \left. \frac{dT}{dr} \right|_R \cdot A$

$\dot{m}_F''' \cdot C_p (T_b - T_u) (1+\beta) \cdot \frac{4}{3} \pi R^3 = +\lambda \frac{(T_b - T_u)}{R} \cdot 4\pi R^2$

$R_c^2 = \frac{3\lambda}{C_p(1+\beta)\dot{m}_F'''} \rightarrow R = \frac{\alpha\sqrt{b}}{S_L}$ as before. $= (\sqrt{6}/2) \delta$

$\rightarrow \left(\frac{2\sqrt{3}}{S_L} \text{ alternative} \right) = (\sqrt{3} \delta \text{ alternative})$

- Find unknown parameter b
- b scales the heat flux at the wall
- Is there one value?
- Use experimental δ , S_L to correlate b
- Use $d = \frac{2\alpha\sqrt{b}}{S_L}$
- Use average α
 - Each fuel at T_{ad} , 300 K
- Plot d vs $2\alpha/S_L \rightarrow b = (\text{slope})^2 = 2.17$
 - Force intercept = 0



Temperature Dependence

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