

Chemical Engineering 374

Fluid Mechanics
Fall 2011

Integral Energy Balance

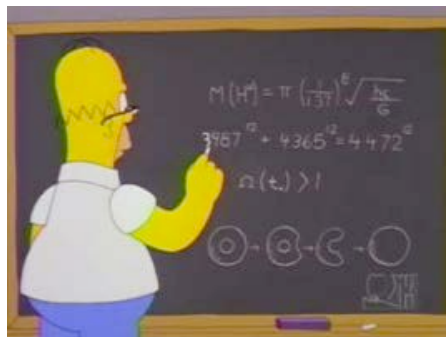


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In this house, we obey the laws of
thermodynamics!

– Homer Simpson



Integral Energy Balance

- Recall, we are writing balance equations.
 - Fluid Statics (no flow)
 - Mass Balance (last time)
 - Energy Balance (today)
 - Momentum Balance (later)
- } Reynolds Transport Theorem

$$\underbrace{\frac{dB_{sys}}{dt}}_{\text{System of fixed Mass (closed system)}} = \underbrace{\frac{d}{dt} \int_{CV} \rho b dV + \int_{CS} \rho b \vec{v} \cdot \vec{n} dA}_{\text{Control Volume: Some (usually fixed) region of space}}$$



System of fixed
Mass (closed system)

Control Volume: Some (usually fixed) region of space

Energy of the system: Internal, Kinetic, Potential

$$E = U + \frac{1}{2}mv^2 + mgz$$

$$e = u + \frac{1}{2}v^2 + gz$$

Conservation law for our system? 1st Law of thermodynamics

$$\frac{dE}{dt} = \frac{dQ}{dt} + \frac{dW}{dt}$$

RTT $\rightarrow B_{sys} = E, b = e$

$$\frac{dQ}{dt} + \frac{dW}{dt} = \frac{d}{dt} \int_{CV} \underbrace{\rho(u + \frac{1}{2}v^2 + gz)}_{\text{Volumetric energy}} dV + \int_{CS} \underbrace{\rho(u + \frac{1}{2}v^2 + gz)\vec{v} \cdot \vec{n} dA}_{\text{Energy flux}}$$



Consider Uniform Properties within a control volume, and Uniform Velocities

$$\frac{dQ}{dt} + \frac{dW}{dt} = \frac{d}{dt} \left[\rho \left(u + \frac{1}{2} v^2 + gz \right) V \right] + \underbrace{\left[\rho v A \left(u + \frac{1}{2} v^2 + gz \right) \right]_{out}}_{\dot{m}} - \left[\rho v A \left(u + \frac{1}{2} v^2 + gz \right) \right]_{in}$$

Pressure is buried in the work term

$$\frac{dW}{dt} : dW = \vec{F} \cdot d\vec{x}$$

Forces at the Surface

W_p – Pressure forces (stress)

W_v – Viscous stresses (usually ignore as small)

Forces internal to the system

W_s – Shaft work (pump, turbine)

W_o – Other (electric, magnetic, surface tension)



W_s is left as is → either specified directly, or computed

Positive when work is done on the system

Negative when system does work on surroundings

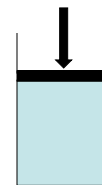
W_p is pressure work, or work to deform the boundary of the SYSTEM

$$dW = F dx = P A dx$$

Consider piston compression

$$\frac{dW}{dt} = P A \frac{dx}{dt} = P A v$$

$$\frac{dW}{dt} = - \int_{CS} P \vec{v} \cdot \vec{n} dA = - \int_{CS} \frac{P}{\rho} \rho \vec{v} \cdot \vec{n} dA$$



General control volume

- P/ρ (=) energy per mass
- Note the negative sign
- This work is the rate of energy flux across the system surface
 - associated with pressure work (deformation).
- This is the rate of energy needed to move the fluid (to move the system)



$$\frac{dQ}{dt} + \frac{dW_s}{dt} - \int_{CS} \frac{P}{\rho} \rho \vec{v} \cdot \vec{n} dA = \frac{d}{dt} \int_{CV} \rho \left(u + \frac{1}{2} v^2 + gz \right) dV + \int_{CS} \rho \left(u + \frac{1}{2} v^2 + gz \right) \vec{v} \cdot \vec{n} dA$$

- Move term to RHS
- Assume uniform properties

$$\frac{dQ}{dt} + \frac{dW_s}{dt} = \frac{d}{dt} \left[\rho \left(u + \frac{1}{2} v^2 + gz \right) V \right] + \left[\rho v A \left(u + \frac{P}{\rho} + \frac{1}{2} v^2 + gz \right) \right]_{out} - \left[\right]_{in}$$

- Multiple streams need multiple terms
- $u + P/\rho = h = u + Pv$



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$$\frac{dQ}{dt} + \frac{dW_s}{dt} = \frac{d}{dt} \left[\rho \left(u + \frac{1}{2} v^2 + gz \right) V \right] + \left[\rho v A \left(u + \frac{P}{\rho} + \frac{1}{2} v^2 + gz \right) \right]_{out} - \left[\right]_{in}$$

Simplify

- Steady State
- $Q=0$ (no heat transfer)
- Constant mass flow
- Constant internal energy (no friction, ΔT , Q)

$$\begin{aligned} \frac{dW_s}{dt} &= \left[\rho v A \left(\frac{P}{\rho} + \frac{1}{2} v^2 + gz \right) \right]_{out} - \left[\rho v A \left(\frac{P}{\rho} + \frac{1}{2} v^2 + gz \right) \right]_{in} \\ &= \dot{m} \Delta e_{mech} = \Delta \dot{E}_{mech} \end{aligned}$$

- Shaft work converted to mechanical energy.
- Mechanical energy is the energy that can be directly converted to mechanical work.
- Ideal, no losses (friction/heat)
- Real systems have losses
- Convenient to consider the ideal case with some efficiency: known or compute.



$$\eta = \frac{E_{mech, real}}{E_{mech, ideal}}$$

$$\eta_{pump} = \frac{\Delta E_{mech}}{W_{shaft}}$$

$$\eta_{turbine} = \frac{W_{shaft}}{\Delta E_{mech}}$$

- Efficiency is positive, so use absolute values if needed.
- Pump/motor, turbine/motor → product of efficiencies



Example 1

Frictionless, Steady, Vertical Pipe Flow

$$\frac{dQ}{dt} + \frac{dW_s}{dt} = \frac{d}{dt} \left[\rho \left(u + \frac{1}{2} v^2 + gz \right) V \right] + \left[\rho v A \left(u + \frac{P}{\rho} + \frac{1}{2} v^2 + gz \right) \right]_{out} - \left[\right]_{in}$$

0 0 0

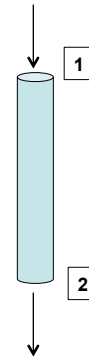
$\Delta u?$

$\Delta v?$

$\Delta m?$

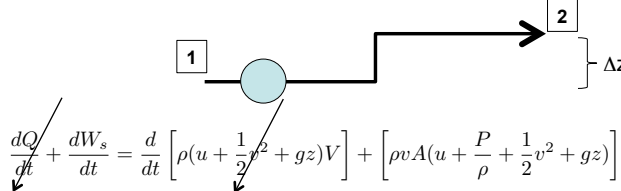
$$\left(\frac{P}{\rho} + gz \right)_{out} = \left(\frac{P}{\rho} + gz \right)_{in}$$

$$(P_2 - P_1) = -\rho g(z_2 - z_1) = \rho g h \quad \text{Our old friend!}$$



Example 2

- Pump liquid through a steady, frictionless nozzle
 - Nozzle, so A_1 not equal to A_2
- Not open to the atmosphere (pipe continues in both directions)



$$\frac{dQ}{dt} + \frac{dW_s}{dt} = \frac{d}{dt} \left[\rho \left(u + \frac{1}{2} v^2 + gz \right) V \right] + \left[\rho v A \left(u + \frac{P}{\rho} + \frac{1}{2} v^2 + gz \right) \right]_{out} - \left[\right]_{in}$$

$0 \qquad \qquad 0 \qquad \qquad \Delta u?$
 $\qquad \qquad \qquad \qquad \Delta v?$
 $\qquad \qquad \qquad \qquad \Delta m?$

$$\frac{\dot{W}_p}{\dot{m}} = \frac{P_2 - P_1}{\rho} + \frac{v_2^2 - v_1^2}{2} + g(z_2 - z_1)$$

What if ends open to the atmosphere?
 What if the inlet and outlet pipes are the same size?

