

ChE 374—Lecture 6—Mass Balance

- Reynolds Transport Theorem: $\frac{B_{sys}}{dt} = \frac{d}{dt} \int_{CV} \rho b dV + \int_A \rho b \vec{v} \cdot \vec{n} dA.$

$\rho b \vec{v} \cdot \vec{n}$ is the flux of B stuff through the control surface.

- Integral Mass Balance

1. $B = M$, $b = B/M = 1$.
2. Apply the conservation law: $dM/dt = 0$: mass is conserved.
3. $\frac{d}{dt} \int_{CV} \rho dV + \int_A \rho \vec{v} \cdot \vec{n} dA = 0$.

- Cases

1. Steady State
2. Constant density
 - * Liquids have approximately constant density
 - * Gas density: ideal gas law: vary pressure (high speed flows or compressor), vary temperature (e.g., combustion), vary moles (e.g., combustion/reaction).
3. Uniform inside C.V. and/or Uniform inlet/outlet flows over surface.
4. Fixed or variable C.V. The control volume C.V. can move
 - * $\vec{v} = \vec{v}_{sys} - \vec{v}_{cv}$.
 - * Can pull the d/dt inside the integral.
$$\frac{dm}{dt} = \dot{m}_{in} - \dot{m}_{out}$$

- Examples

- Simple flow with change in area of inlet/outlet.
 - * Fixed CV, SS, Constant ρ , Uniform Flows.
- Filling a tank with inlet and outlet.
 - * Constant ρ , Uniform Flows, not S.S., none-fixed C.V.
- Nonuniform flow → compute the average velocity from a velocity profile.

- Differential Form of Mass Balance.

- Get from the Integral form with a small/uniform property control volume and shrink to a point.
- Get from the Gauss Divergence Theorem.

(1)

Class 6 - Integral Mass Balance.

$$\text{R.T.T. : } \frac{dB_{sys}}{dt} = \frac{d}{dt} \int_{cv} \rho b dV + \int_{cs} \rho_b \vec{v} \cdot \vec{n} dA$$

Integral Mass Balance.

$$(1) B = M \text{ (kg)}$$

$$b = \frac{B}{M} = 1$$

$$\rightarrow \frac{dM}{dt} = \frac{d}{dt} \int_{cv} \rho dV + \int_{cs} \rho \vec{v} \cdot \vec{n} dA$$

$$(2) \text{ Apply Conservation}$$

$$\text{law } \frac{dM}{dt} = 0$$

$$\rightarrow \boxed{\frac{d}{dt} \int_{cv} \rho dV + \int_{cs} \rho \vec{v} \cdot \vec{n} dA = 0}$$

That's it!

Cases

(1) S.S. \rightarrow nothing changes at a given point

$$\frac{d}{dt} \int_{cv} \rho dV = \frac{dM_{cv}}{dt} = 0 \text{ at S.S.}$$

$$\rightarrow \int_A \rho \vec{v} \cdot \vec{n} dA = 0$$

(2) Const ρ \rightarrow \div through by ρ , $\int_{cv} dV = V$

$$\rightarrow \frac{dV_{cv}}{dt} + \int_{cs} \vec{v} \cdot \vec{n} dA = 0$$

if the C.V. is fixed then $\int_{cs} \vec{v} \cdot \vec{n} dA = 0$

- Liq: $\rho \approx \text{const.}$

- Gases $P = MP/RT \rightarrow P, T, M \text{ vary}$

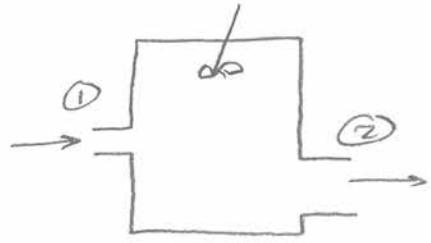
- High Speed flow \rightarrow high ΔP

- Reactions $\rightarrow \Delta T, \Delta n_{moles} \rightarrow \Delta M$

- For low speed, \approx Isothermal, $P_{gas} \approx \text{const.}$

(2)

- (3) Uniform Props inside C.V.
Uniform inlets, outlets



$$\frac{d}{dt} \int_{cv} \rho dV + \int_{cs} \rho \vec{V} \cdot \hat{n} dA = 0$$

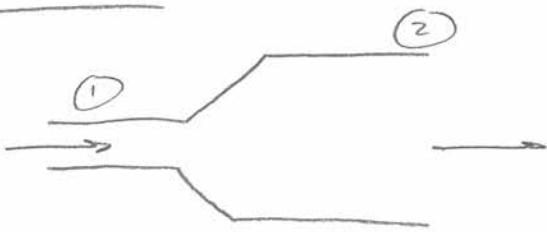
$$\frac{d \rho V}{dt} + (\rho V A)_{out} - \underbrace{(\rho V A)_{in}}_m = 0$$

$\vec{V} \cdot \hat{n} @ ①$ is neg
 $\vec{V} \cdot \hat{n} @ ②$ is pos

$$\frac{d M_w}{dt} = m_{in} - m_{out}$$

V, P can change in time.

Example 1



water, S.S.

Q: Fixed C.V. $\rightarrow Y$

Q: SS $\rightarrow Y$

Q: Const P $\rightarrow Y$

Q: Unif in/out $\rightarrow Y$.

$$S.S. \rightarrow \int_{cs} \rho \vec{V} \cdot \hat{n} dA = 0$$

$$\text{Const } P \rightarrow \int_{cs} \vec{V} \cdot \hat{n} dA = 0$$

$$\text{Uniform} \rightarrow V_2 A_2 - V_1 A_1 = 0$$

$$\begin{aligned} & \text{or } V_2 A_2 = V_1 A_1 \\ & \text{or } (\rho A V)_1 = (\rho A V)_2 \end{aligned}$$

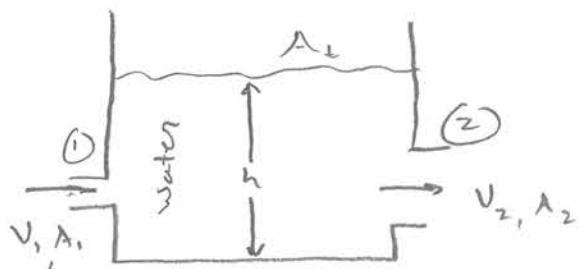
$$\rightarrow m_{in} = m_{out}$$

$$\text{or } \dot{V}_{in} = \dot{V}_{out}$$

$$V_2 = V_1 \frac{A_1}{A_2}$$

Volume flow in = Volume flow out.

(3)

Example 2Given V_1, V_2, A_1, A_2, A_t
Find $h(t)$ 

Q: Fixed C.V. ? $\rightarrow N$
Take C.V. = water in Tank

Q: const ρ ? $\rightarrow Y$
Q: Uniform? $\rightarrow Y$
Q: SS? $\rightarrow N$

$$\text{const } \rho \rightarrow \frac{dV}{dt} + \int_A \vec{v} \cdot \vec{n} dA = 0$$

$$\text{Unif } \rightarrow \frac{dV}{dt} + V_2 A_2 - V_1 A_1 = 0$$

$$\nabla V = A_t h, \rightarrow \div \text{ by } A_t, \text{ rearrange}$$

$$\frac{dh}{dt} = \underbrace{\left(\frac{V_1 A_1 - V_2 A_2}{A_t} \right)}_{\text{const } c}$$

$$\text{Solve } \rightarrow h = h_0 + \left(\frac{V_1 A_1 - V_2 A_2}{A_t} \right) t$$

Suppose $V = V(h)$?

$V = V(t)$?

insert in ODE then solve ODE

* Always Try to align The C.V., C.S. to be \perp to The Velocities

Example : Nonuniform Flow

$$\nabla V = VA \rightarrow d\nabla V = V dA \rightarrow \nabla V = \int V dA$$

$$\bar{V} = \frac{1}{A} \int V dA \rightarrow \nabla V = \int V dA = A \bar{V}$$

Given a velocity profile, Find $\bar{V} = \frac{1}{A} \int V(x) dA$

(4)

- Plug in Given $v(x)$, Set dA , Such as $dA = wdx$
- Integrate.

Differential Mass Balance.

Fixed C.V., uniform

$$\frac{d}{dt} \int_{CV} \rho dV + \int_{CS} \rho \vec{v} \cdot \vec{n} dA = 0$$

$$\downarrow \frac{\partial \rho}{\partial t} + \rho u_2 \Delta y - \rho_{x_1} u_1 \Delta y + \rho v \Delta x - \rho_{y_1} v \Delta x = 0$$

$\Delta x, \Delta y$

here Areas are $\Delta x, \Delta y$ for a unit Δz in the Page.

$$\therefore \Delta x, \Delta y \rightarrow \frac{\partial \rho}{\partial t} + \frac{\rho_{x_2} u_2 - \rho_{x_1} u_1}{\Delta x} + \frac{\rho_{y_2} u_2 - \rho_{y_1} v_1}{\Delta y} = 0$$

$$\lim \Delta x, \Delta y \rightarrow 0 \rightarrow \frac{\partial \rho}{\partial t} + \frac{\partial \rho u}{\partial x} + \frac{\partial \rho v}{\partial y} = 0$$

$$\rightarrow \boxed{\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \vec{v} = 0}$$

Optional

Gauss Divergence Theorem (GDT)

$$\int_A \vec{V} \cdot \vec{n} dA = \int_{CV} \nabla \cdot \vec{V} dV \equiv GDT$$

Then

$$\frac{d}{dt} \int_{CV} \rho dV + \int_{CS} \rho \vec{v} \cdot \vec{n} dA = 0$$

$$\rightarrow \frac{d}{dt} \int_{CV} \rho dV + \int_{CV} \nabla \cdot (\rho \vec{v}) dV = 0$$

$$\rightarrow \int_{CV} \left(\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{v}) \right) dV = 0$$

$$\rightarrow \boxed{\frac{\partial \rho}{\partial t} + \nabla \cdot \rho \vec{v} = 0}$$

