

# Chemical Engineering 374

## *Fluid Mechanics*

### Exam 3 Review



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## Exam Review, By Content/Lectures

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- Classes 25-32 (plus review)
- Environmental
- Chapter 6.1-6.4                      Momentum Balance
- Chapter 9.1-9.2, 9.4-9.6      Differential Balances
- Chapter 10.6                          Boundary Layers
- Chapter 11.1-11.6                  External Flows: Drag
- Chapter 14.1-14.5                  Pumps and Turbines
- HW 19-27



## Class 25—Integral Momentum Balance

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- Force Balance 
$$\sum \vec{F} = \frac{dm\vec{v}}{dt} + \sum (\dot{m}\vec{v})_{out} - \sum (\dot{m}\vec{v})_{in}$$
  - $\dot{m}$  is not a vector
  - Forces are external: body and surface (esp. P)
  - Decompose into scalar directions
    - One equation in one unknown (force, etc.)
    - Signs matter!
- Pick control volume intelligently
- Pressure surface forces should be gauge (unless account for full absolute pressure (including atm) on all surfaces.)
- For nonuniform flows, may have to integrate to get the full terms in the force balance, but the principle is the same.



## Class 26—Differential Balances

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- Mass Balance
- Momentum Balance 
$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \vec{v}) = 0 \quad \nabla \cdot \vec{v} = 0$$
- Derived from the RTT
- Continuity Equation
  - Used as a constraint for velocity
  - Book/handouts give expanded forms for Cartesian, Cylindrical, Spherical coordinates.
  - Incompressible (const  $\rho$ ) means rate in = rate out.
  - If rate in  $\neq$  rate out then the density is changing.
- Momentum equation: just a differential force balance
  - (accum) = (in)-(out) + (body and surface forces)
  - Book/handouts give expanded forms in three coordinates
  - Again, use to find velocity field or pressure field.



## Class 27—Navier-Stokes Equations

$$\frac{\partial \vec{v}}{\partial t} + \vec{v} \cdot \nabla \vec{v} = -\frac{1}{\rho} \nabla P + \nu \nabla^2 \vec{v} + \vec{g}$$

- Incompressible, Newtonian, vector
- The equations look scary, but we seriously simplify them
  - Know how to drop out terms:
- Solution procedure:
  - Is it steady? (usually, here), is it compressible (no, usually here const  $\rho$ ), is it 1-D? (yes, usually here).
  - 1D  $\rightarrow$  one momentum equation (one component of the vector expression).
  - 1D  $\rightarrow$  maybe vary in y direction, but may have only  $u_x$  velocity (still 1-D)
    - Use only x-momentum, but varies in y-direction.
  - Solve for a velocity component OR...
  - Given a velocity field, can solve for the pressure field.
- Boundary conditions
  - Velocity (mass flow) given at some point (inflow/outflow)
  - Velocity zero at walls.
  - Symmetry (like at centerlines)  $\rightarrow$  velocity gradients are zero.
  - Air/liquid interface  $\rightarrow$  no shear  $\rightarrow$  velocity gradient zero.



## Class 28—Boundary Layers

- Mostly conceptual here.
  - Euler equations (Navier-Stokes without viscosity) far from walls.
  - Boundary layer equations near walls (Simplified Navier-Stokes equations).
- Boundary Layer results.
  - Boundary layers have two length scales (length along the plate, and thickness).
  - Boundary layers are very thin compared to length. (So Euler equations solved ignoring BL thickness)
  - Thin, relatively parallel streamlines imply no pressure gradient normal to the plate. (Then the pressure gradient along the plate is that in the free stream (=0 for flat plate BL).
  - Navier-stokes (or x-mom) told us there are two length scales.
  - Continuity told us the scaling for v-velocity.
  - Y-momentum told us there is no pressure gradient normal to the plate.
  - X-momentum then lost a viscous term ( $du/dx$ ), and  $dp/dx$  written in terms of  $dU/dx$  with Bern. Eq.
- Computed BL thickness
- Transition for laminar and turbulent Reynolds numbers (5E5 is the engineering cutoff).
- BL grows with distance, Re grows with distance  $\rightarrow$  becomes turbulent.
- Shear stress decreases with distance.
- Turbulent shear > laminar shear.



RECALL HOW WE USE THESE FACTS, remember the 2 plate direction prob.

## Class 29—External Flow

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- Lift, Drag, Drag Coefficient.
- Drag is emphasized and is the net force in flow direction.
  - Pressure forces (form drag)
    - Flow separation
  - Viscous forces (friction drag)
  - Streamlining reduces pressure drag, but increases friction drag, but usually, pressure drag dominates.
- $F = C_d \rho v^2 A / 2$ 
  - A is the projected area, or the planview area
  - Use Table 11-1, 11-2 (given on exam if needed)
  - If v is unknown, guess laminar or turbulent  $\rightarrow C_d \rightarrow v \rightarrow Re \rightarrow$  confirm or adjust  $C_d$ . (Tables  $\rightarrow$  only one try needed)
  - For small particles guess laminar, for big objects, guess turbulent.
- Terminal velocity follows from a force balance. Object falls under gravity until forces balance: buoyant, weight, drag



## Class 30—Pumps

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- Pump types: Positive displacement, dynamic.
- Dynamic = Centrifugal, Mixed Flow, Axial.
- bhp, efficiency.  $\rho * g * Q * H / \text{bhp}$
- Pump performance curves (PPC): Head versus Flow
  - Shutoff head, free delivery flow rate, intermediate.
  - Individual pump whether alone, series or parallel operates on PPC.
  - System curve is system head versus flow.
  - Operating point where the SC and PPC intersect.
- Pump selection: size for required flow/head, maximize  $\eta$ , may have to overspecify pump (higher flow for given head)
- NPSH.
  - Specified for given pump.
  - Lookup  $P_{\text{vap}}$  for given flow. Flow parameters  $\rightarrow P_2, v_2$ . Vary operation to ensure greater than NPSH. (Pressure drops prior to pump may lead to cavitation if  $\text{NPSH}_{\text{have}} < \text{NPSH}_{\text{need}}$ ).



## Class 31—Pump Scaling

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- Series and Parallel
- Series, increase head for given flow.
  - PPC is sum (vertically) of individual pumps PPC
  - Don't operate beyond Free Delivery Flow for smallest pump, or shutoff/bypass that pump.
  - Can act as a head loss above the free delivery flow.
  - Know how the series pumps work with respect to a system demand curve
- Parallel, increase flow for given head.
  - PPC is sum (horizontally) of individual pumps PPC.
  - Don't operate beyond the shutoff head for the smallest pump, or bypass that pump.
  - Backflow above the shutoff head.
  - Each pump operates on its own PPC, but combined system operates on the combined PPC.
  - But the head over each pump is equal → provides a link (horizontal line on PPC) between individual and combined PPC
  - Again, know how this works on a system curve
- Scaling:
  - $C_H, C_p, \eta = f(C_Q, Re, \epsilon/D) \sim f(C_Q)$ .  $gH, bhp, \eta = f(D, Q, \omega, \rho, \mu, \epsilon)$
  - To scale, as usual, match these groups. Often, keeping one or several parameters const → simplifies the problem.
- Choose pumps based on value of  $N_{sp}$ 
  - if you were given a set of requirements, know how to compute  $N_{sp}$  and choose a pump or turbine.



## Class 32—Turbines

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- Types: Hydraulic, wind, steam, gas, etc.
- Positive displacement, Dynamic
- Dynamic
  - Impulse (Pelton Wheel)
  - Reaction (like inverse pump)
- Pelton Wheel Analysed using momentum balance
- Reaction turbines:
  - Francis (Radial/mixed flow)
  - Kaplan (Axial flow)
- $\eta = 1/\eta_{\text{pump}}$
- Wind turbine
  - Work available,  $\eta = C_p < 0.59$  (more like 0.45)
- Scaling laws are like pumps:  $C_H, C_Q, C_p, \eta$
- Take  $C_p$  as independent parameter
- Turbine selection, based on  $N_{sp}$ .

