

ChE 374–Lecture 31–Pump Scaling

- Series and parallel pumps:
 - Series
 - * Goal: provide greater head for the same flow rate
 - * $H_{tot} = H_1 + H_2$
 - * Pump performance curve is the vertical sum of each individual pump
 - * $bhp_{tot} = bkp_1 + bkp_2$ at the operating point
 - * Issues: If the pumps are not the same capacity, then if the flow is too large, the smaller pump may operate beyond its free delivery flow rate (beyond where its H drops to zero). At that point, the pump acts as a loss, not a gain in head, and damage may result. In this case, shut off the pump and bypass it with a valve. This is not a problem for equal sized pumps.
 - Parallel
 - * Goal: increase \dot{V} for the same head
 - * Pump performance curve is the horizontal sum of each individual pump
 - * $H_1 = H_2$
 - * $\dot{V}_{tot} = \dot{V}_1 + \dot{V}_2$
 - * $bhp_{tot} = bkp_1 + bkp_2$ at the operating point
 - * $\dot{W}_{whp} = \rho g \dot{V} H_{tot}$
 - * $\eta = \rho g \dot{V} H_{tot} / bhp_{tot}$
 - * Issues: Different sized pumps: if head is greater than the shutoff head of the smaller pump, then the flow may actually reverse through the pump, resulting in damage. In that case, bypass the pump with a valve. This is not a problem for equal sized pumps.
- Pump Scaling
 - Often have a pump and want to change the operation, or run with different fluids, or design for different conditions.
 - Know the scaling laws
 - Use dimensional analysis
 - * Pump parameters: $D, \dot{V}, \omega, \rho, \mu, \epsilon$.
 - 6 parameter - 3 dimensions = 3 Π 's
 - $C_Q = \dot{V} / \omega D^3, Re = \rho \omega D^2 / \mu, \epsilon / D$.
 - * Pump properties (depend on the params): Head (H), Power (bhp), Efficiency (η), NPSH.
 - Nondimensionalize these too, using the pump parameters
 - Head, $gH / \omega^2 D^2 = C_H = f(C_Q, Re, \epsilon / D)$
 - Power, $bhp / \rho \omega^3 D^5 = C_P = f(C_Q, Re, \epsilon / D)$
 - Efficiency, $\rho g \dot{V} H / bhp = \eta = f(C_Q, Re, \epsilon / D)$.
 - The effect of Re is small at high Re , like it is for pipes.
 - Small effect of ϵ / D , so the main dependency is on C_Q .
 - See the affinity laws on page 803.
- Pump selection
 - Pump specific speed (N_{sp}) is used to select pumps.
 - * $N_{sp} = C_Q^{1/2} / C_H^{3/4}$
 - Careful of units, its often defined with inconsistent sets of units.
 - Plot η_{max} versus N_{sp} for several pump types.
 - * Choose centrifugal for $N_{sp} < 1.5$, mixed for $1.5 < N_{sp} < 3.5$, and axial for $N_{sp} > 3.5$.
 - Here, N_{sp} is the U.S. version.

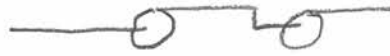
Class 31 - Pumps (2)

Example from last class : NPSH : 14-60 (see attached)

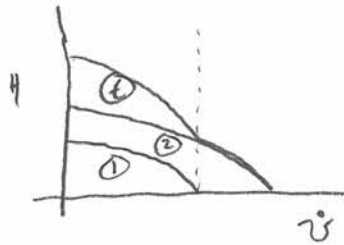
Pumps in Series and parallel

Series

Goal: provide greater head for same flow rate



- $H_{tot} = H_1 + H_2$
- Pump performance curve is the vertical sum of each
- $bhp_{tot} = bhp_1 + bhp_2$ at operating point.



Issues : If pumps are not same capacity, then if flow is too large, the smaller pump may operate beyond its free delivery flow rate (beyond where its H drops to zero). At that point, pump acts as a loss not a gain, may damage

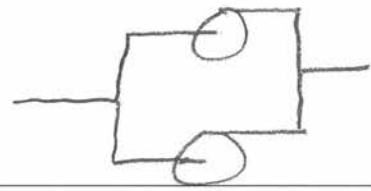
→ Shut it off and bypass.

(not a problem for 2 equal pumps)

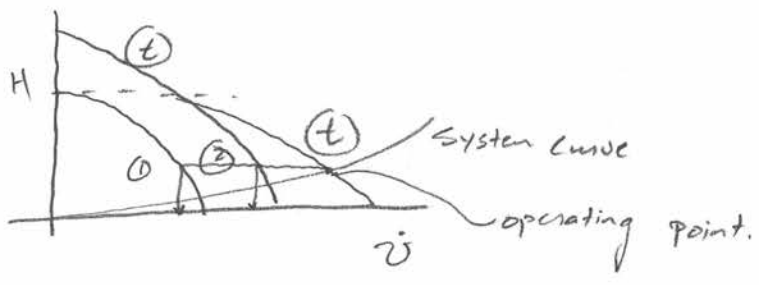


Parallel

- Goal: increase \dot{V} for same head.



- $H_1 = H_2$
- $\dot{V}_t = \dot{V}_1 + \dot{V}_2$
- Pump perf. Curve is the horizontal sum of each pump.



- $bhp_t = bhp_1 + bhp_2$
- $\dot{W}_{WHP} = \rho g \dot{V} H_{tot}$
- $\eta = \frac{\rho g \dot{V}_{tot} H_t}{bhp_{tot}}$

- Issues: Different Size Pumps.
 - if head is greater than the shutoff head of the smaller pump, then the flow may actually reverse through the pump \rightarrow Damage
 - In that case, Bypass the pump with a valve.
 - Not a problem for equal pumps.

Pump Sealing

- Often Have a pump, want to change operation,
or run different fluids
or design for different conditions.
→ Know Scaling Laws.

• Use Dimensional Analysis.

• Pump parameters: $D, \dot{V}, \omega, \rho, \mu, \epsilon$
6 params - 3 Dims = 3 Π 's

• Pump Properties: Head, Power, efficiency, NPSH
(depend on Pump Params)
 $H, \text{bhp}, \eta, \text{NPSH}$
→ Non-Dim These too, using Pump params.

• Pump Params → $C_Q = \frac{\dot{V}}{\omega D^3}$
 $Re = \frac{\rho \omega D^2}{\mu} = \frac{\rho D (\omega D)}{\mu}$
 ϵ/D

• Pump Properties

Head → $\frac{H}{\omega^2 D^3 / g} = C_H = f(C_Q, Re, \frac{\epsilon}{D})$

Power → $\frac{\text{bhp}}{\rho \omega^3 D^5} = C_P = f(C_Q, Re, \frac{\epsilon}{D})$

efficiency → $\frac{\rho g \dot{V} H}{\text{bhp}} = \eta = f(C_Q, Re, \frac{\epsilon}{D})$

- High Re → small effect (as for pipes)
- ϵ/D → small effect.
- See Affinity Laws on p 803.

- to Scale pumps, match the Groups.

Example

- A pump's rpm Doubles : $\omega \rightarrow 2\omega$
- What happens to its Head, Power if C_Q is const?

$$C_Q = \frac{Q}{\omega D^3} ; \quad 2\omega \rightarrow 2Q$$

$$C_H \rightarrow \frac{H_1}{H_2} = \left(\frac{\omega_1}{\omega_2}\right)^2 \rightarrow 2\omega \rightarrow 4H$$

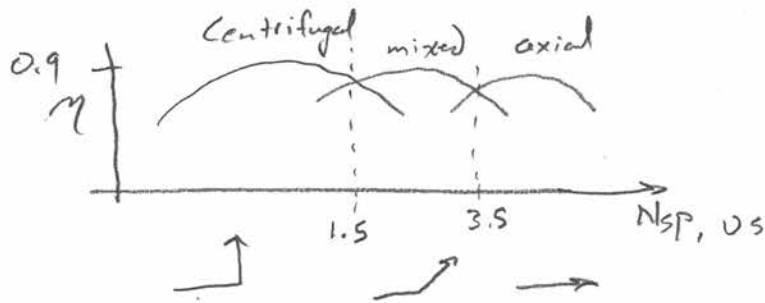
$$C_P \rightarrow \frac{bhp_1}{bhp_2} = \left(\frac{\omega_1}{\omega_2}\right)^3 \rightarrow 2\omega \rightarrow 8bhp.$$

Pump Selection

Pump Specific Speed used to Select Pumps.

$$N_{sp} = C_Q^{1/2} / C_H^{3/4}$$

Plot η_{max} vs N_{sp} for several pump types :



- Careful of Units, See Tbook.

14-60

Water @ 77°F

D = 1.2 in

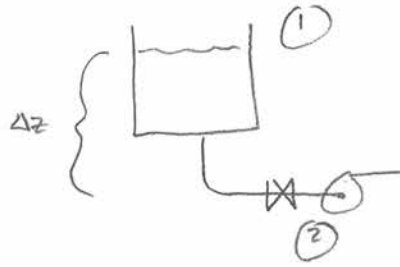
L = 12 ft.

K = 0.5 + 0.3 + 6

$\rho = 62.244 \text{ lbm/ft}^3$

$\mu = 6.0016 \times 10^{-4} \text{ lbm/ft}\cdot\text{s}$

$\Delta z = 20 \text{ ft.}$



$$\text{NPSH} = 1 + 0.0054 Q^2 \quad \text{ft w/ } Q(\text{=}) \frac{\text{gal}}{\text{min}}$$

$$P_{\text{sat}} = 0.46407 \text{ lbf/in}^2$$

Max flow w/o Cavitation.

$$\frac{P_2 - P_1}{\rho g} + \frac{V_2^2 - V_1^2}{2g} + g(z_2 - z_1) = -\frac{fLV^2}{2Dg} - \frac{KV^2}{2g}$$

$$\text{NPSH} = \frac{P_2}{\rho g} + \frac{V_2^2}{2g} - \frac{P_{\text{sat}}}{\rho g}$$

$$\frac{P_2}{\rho g} + \frac{V_2^2}{2g} = z_1 - \frac{fLV^2}{2Dg} - \frac{KV^2}{2g} + \frac{P_1}{\rho g}$$

$$\text{NPSH} = z_1 - \frac{fLV^2}{2Dg} - \frac{KV^2}{2g} - \frac{P_{\text{sat}} + P_1}{\rho g} = 1 + 0.0054 Q^2$$

$$z = 20 \text{ ft}$$

$$L = 12 \text{ ft}$$

$$D = 0.1 \text{ ft}$$

$$g = 32.17 \text{ ft/s}^2$$

$$P_{\text{sat}} = 2149.8 \text{ lbm/ft}\cdot\text{s}^2$$

$$P_1 = 68078.7 \text{ lbm/ft}\cdot\text{s}^2$$

$$= 1 + 1087.8 Q^2 \quad \text{ft}^3/\text{s}$$

$$Q = \frac{\pi}{4} D^2 V$$

$$\frac{1}{\sqrt{f}} = -2 \log \left(\frac{2.51}{\text{Re} \sqrt{f}} \right)$$

Solve w/ Mathcad → 56.6 gpm